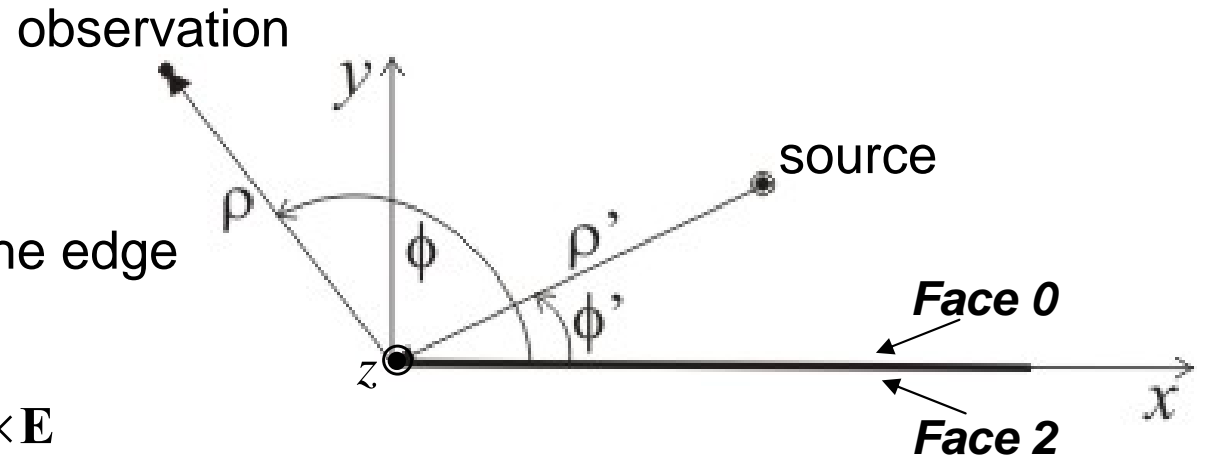

Scattering from a perfectly conducting half-plane

RADIATION FROM THE HALF PLANE

Assumptions:

1. normal incidence
2. electric line source
3. source far from the vertex of the edge



$$E_z = -\frac{\omega\mu I_e}{4} G; \quad H_z = -\frac{1}{j\omega\mu} \nabla \times \mathbf{E}$$

Green's function

$$G = \sqrt{\frac{2j}{\pi k \rho'}} e^{-jk\rho'} F(k\rho)$$

Modal solution

$$F(k\rho) = \frac{1}{2} \sum_{m=0}^{\infty} \epsilon_m J_{m/2}(k\rho) e^{j(m/2)(\pi/2)} \left[\frac{m}{2} \cos \Phi^- \pm \frac{m}{2} \cos \Phi^+ \right]; \quad \epsilon_m = \begin{cases} 0 & m=0 \\ 1 & m \neq 0 \end{cases} \quad \Phi^\mp = (\phi \mp \phi')$$

hard *soft*

Rapidly convergent for $k\rho < 1$ (about 15 terms)
 for $1 < k\rho < 10$ (about 40 terms)
 Slowly convergent for $k\rho > 10$

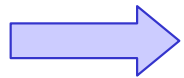
High frequency asymptotic expansion

HIGH FREQUENCY ASYMPTOTIC EXPANSION



Converting the infinite series into an integral

$$F(k\rho) = \int_{C_\alpha} S(\alpha) e^{k\rho f(\alpha)} d\alpha$$



deformation onto SDP



finding saddle points and poles

How to do:

1. Expansion of cosine terms into complex exponentials
2. Integral expression for Bessel functions
3. Exchanging the order of summation and integration

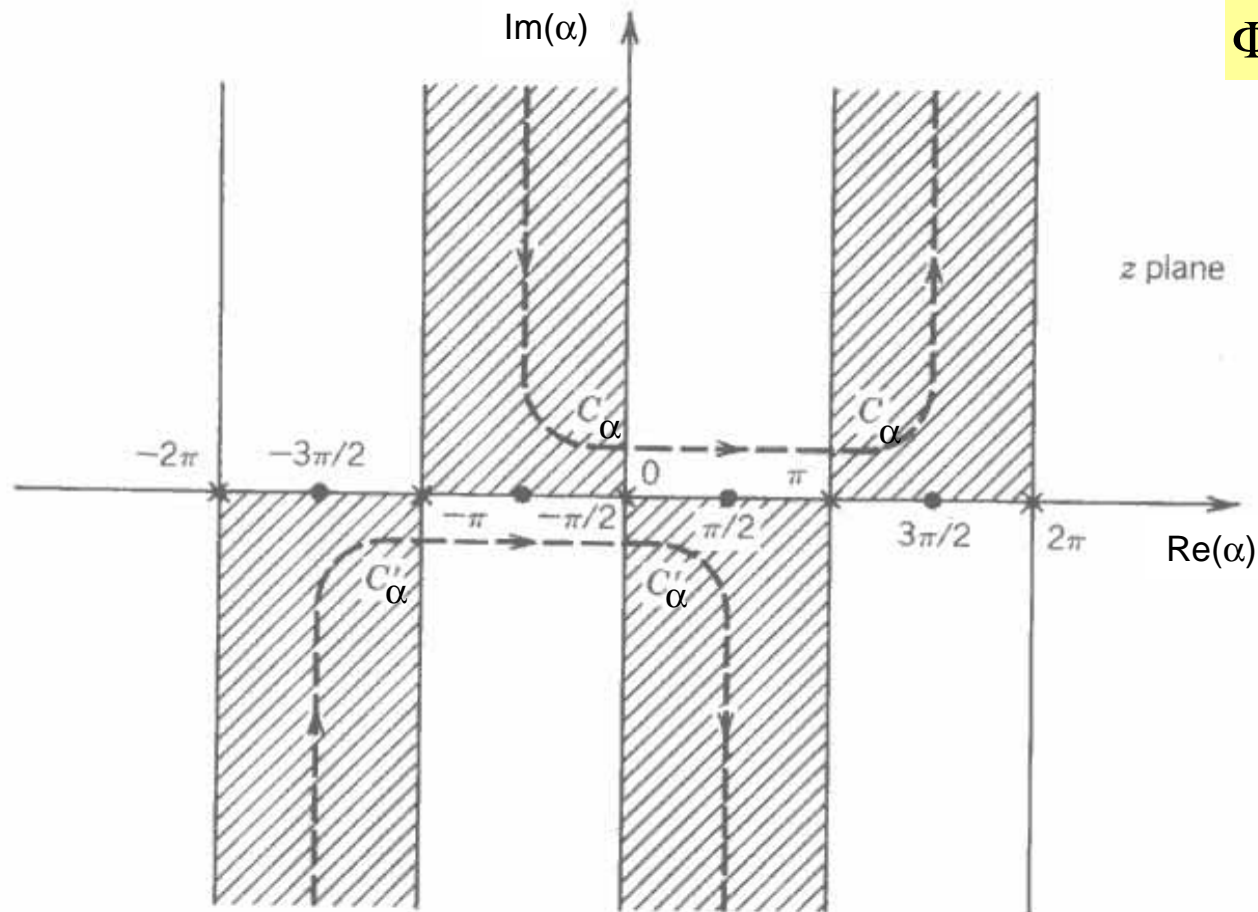
HIGH FREQUENCY ASYMPTOTIC EXPANSION

$$F(k\rho) = F_1(k\rho) \pm F_2(k\rho)$$

$$F_i(k\rho) = \frac{1}{8\pi j} \int_{C_{\alpha'}^{-} C_{\alpha}} S_i(\alpha) e^{k\rho f_i(\alpha)} d\alpha \quad \text{where} \quad \begin{cases} S_1(\alpha) = \cot\left(\frac{\Phi^- + \alpha}{4}\right) \\ S_2(\alpha) = \cot\left(\frac{\Phi^+ + \alpha}{4}\right) \end{cases} \quad \text{and} \quad f_1(\alpha) = f_2(\alpha) = j \cos \alpha$$

$$\Phi^- = \phi - \phi'$$

$$\Phi^+ = \phi + \phi'$$

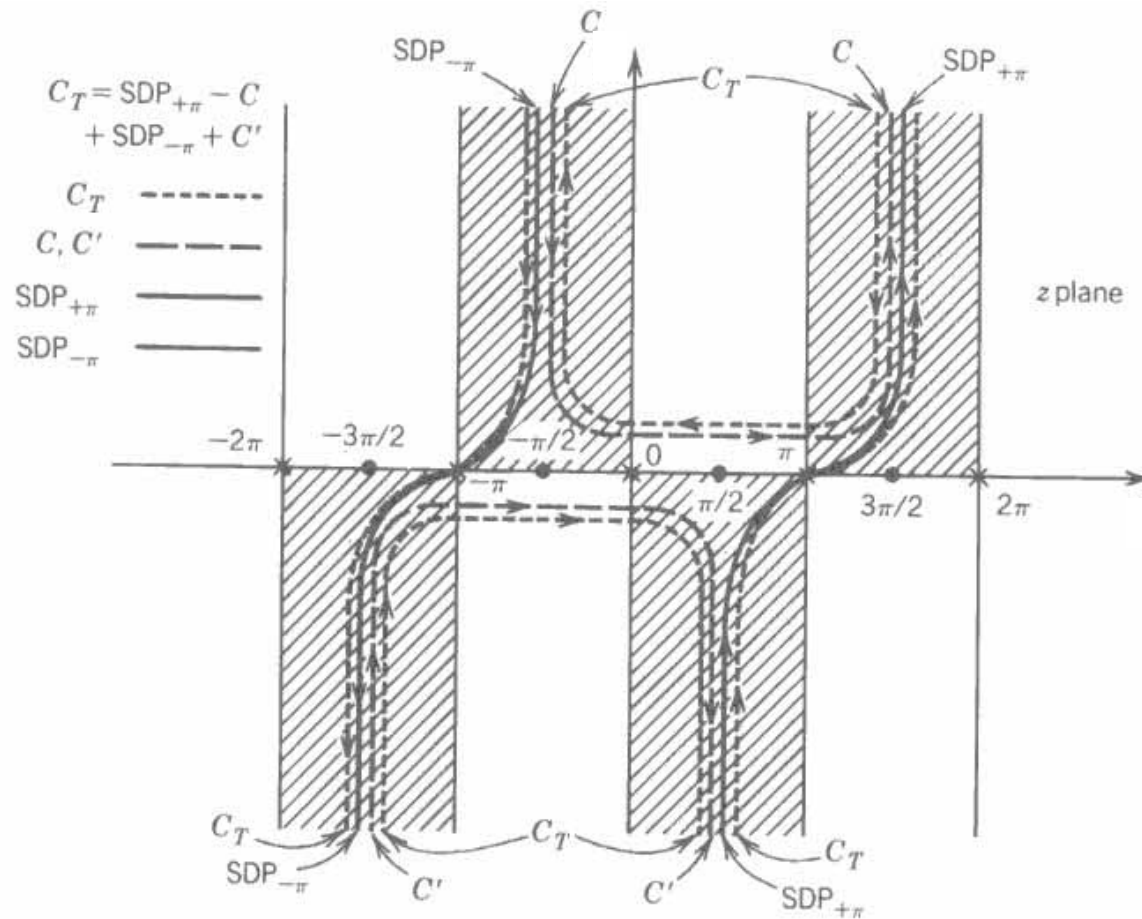


HIGH FREQUENCY ASYMPTOTIC EXPANSION

1. Choice of closed contour

$$C_T = C_{\alpha'} + SDP_{+\pi} - C_{\alpha} + SDP_{-\pi}$$

$$\begin{aligned} F_1(k\rho) &= \frac{1}{8\pi j} \int_{C_{\alpha'} - C_{\alpha}} S_1(\alpha) e^{k\rho f_1(\alpha)} d\alpha = \\ &= \frac{1}{8\pi j} \oint_{C_T} S_1(\alpha) e^{k\rho f_1(\alpha)} d\alpha - \frac{1}{8\pi j} \int_{SDP_{+\pi}} S_1(\alpha) e^{k\rho f_1(\alpha)} d\alpha - \frac{1}{8\pi j} \int_{SDP_{-\pi}} S_1(\alpha) e^{k\rho f_1(\alpha)} d\alpha \end{aligned}$$



RESIDUES CONTRIBUTION

2. From $\oint = \text{residues of the poles inside } C_T$

$$\frac{1}{8\pi j} \oint_{C_T} S_1(\alpha) e^{k\rho f_1(\alpha)} d\alpha = 2\pi j \sum_{i=1}^{Np} \text{Re } s(\alpha_i) U(\alpha_i)$$

3. Poles of $S_1(\alpha) \longrightarrow \cot\left(\frac{\Phi^- + \alpha}{4}\right) \Rightarrow \left(\frac{\Phi^- + \alpha}{4}\right) = \pi N \quad N = 0, \pm 1, \pm 2, \dots$

Easy calculation

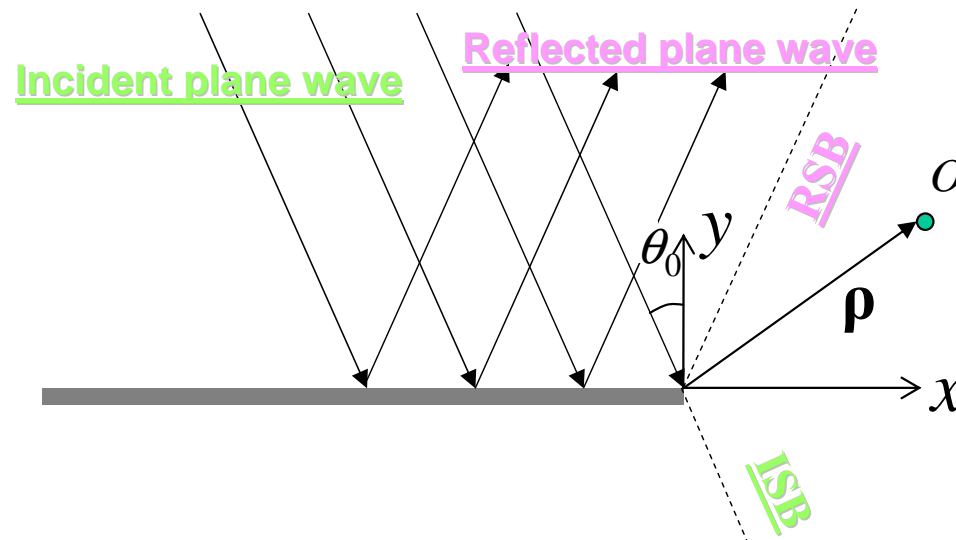
$\alpha = -\Phi^- + 4\pi N$ real poles

Incident GO

$$2\pi j \sum_{i=1}^{Np} \text{Re } s(\alpha_i) U(\alpha_i) = e^{jk\rho\Phi^-} U(\pi - \Phi^-)$$

Reflected GO

$$2\pi j \sum_{i=1}^{Np} \text{Re } s(\alpha_i) U(\alpha_i) = e^{jk\rho\Phi^+} U(\pi - \Phi^+)$$



SDP CONTRIBUTION

4. Non uniform asymptotic approximation (isolated poles – saddle points)

$$\frac{1}{8\pi j} \int_{SDP_{+\pi}} S_1(\alpha) e^{-jk\rho \cos \alpha} d\alpha \quad + \quad \frac{1}{8\pi j} \int_{SDP_{-\pi}} S_1(\alpha) e^{-jk\rho \cos \alpha} d\alpha$$

$$A \int_{SDP} f(z) e^{\Omega q(z)} d\alpha \approx A \sqrt{\frac{2\pi}{\Omega q''(z_s)}} f(z_s) e^{\Omega q(z_s)}$$

Asymptotic evaluation parameters

<u>integrand</u>	<u>expansion argument</u>	<u>phase function</u>	<u>saddle point</u>
$f(z) = S_1(\alpha)$	$\Omega = k\rho$	$q(z) = -j \cos \alpha$	$q'(z) = j \sin \alpha = 0$
			$z_s = \alpha_s = \pm \pi$
$\alpha_s = +\pi$			$\alpha_s = -\pi$

$$\frac{e^{-j\pi/4}}{4\sqrt{2\pi}} \cot\left(\frac{\pi + \Phi^-}{4}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} \quad + \quad \frac{e^{-j\pi/4}}{4\sqrt{2\pi}} \cot\left(\frac{\pi - \Phi^-}{4}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}}$$

$$F_{1SDP}(k\rho) \approx \frac{e^{-j\pi/4}}{2\sqrt{2\pi}} \frac{1}{\cos\left(\frac{\Phi^-}{2}\right)} \frac{e^{-jk\rho}}{\sqrt{k\rho}}$$

SDP CONTRIBUTION

Equivalently...

$$\frac{1}{8\pi j} \int_{SDP_{+\pi}} S_2(\alpha) e^{-jk\rho \cos \alpha} d\alpha$$

+

$$\frac{1}{8\pi j} \int_{SDP_{-\pi}} S_2(\alpha) e^{-jk\rho \cos \alpha} d\alpha$$

$$F_{2SDP}(k\rho) = \frac{e^{-j\pi/4}}{2\sqrt{2\pi}} \frac{1}{\cos\left(\frac{\Phi^+}{2}\right)} \frac{e^{-jk\rho}}{\sqrt{k\rho}}$$

Summary of the non-uniform first order asymptotic evaluation

$$F(k\rho) = \frac{-e^{-j\pi/4}}{2\sqrt{2\pi}} \left[\frac{1}{\cos\left(\frac{\Phi^-}{2}\right)} \pm \frac{1}{\cos\left(\frac{\Phi^+}{2}\right)} \right] \frac{e^{-jk\rho}}{\sqrt{k\rho}} + e^{jk\rho\Phi^-} U(\pi - \Phi^-) \pm e^{jk\rho\Phi^+} U(\pi - \Phi^+)$$

SDP CONTRIBUTION

5. Uniform asymptotic approximation (poles near saddle points)

$$\frac{1}{8\pi j} \int_{SDP_{+\pi}} S_1(\alpha) e^{-jk\rho \cos \alpha} d\alpha \quad + \quad \frac{1}{8\pi j} \int_{SDP_{-\pi}} S_1(\alpha) e^{-jk\rho \cos \alpha} d\alpha$$

6. Pauli – Clemmow modified method of steepest descent path

6a. Expansion of the phase term $f(\alpha) = f(\alpha_s) - \mu^2$

6b. Expansion of the integrand $F(\mu) = S_1(\alpha) [f(\alpha) - f(\alpha_i)] \frac{d\alpha}{d\mu} = \sum_{m=0}^{\infty} c_m \mu^m$

6c. Assuming $f(\alpha) - f(\alpha_i) = f(\alpha_s) - f(\alpha_i) - \mu^2 = -(\mu^2 + ja)$; $a = j[f(\alpha_s) - f(\alpha_i)]$

6d. Change of integration variable

$$\int_{-\infty}^{\infty} \frac{e^{-k\rho\mu^2}}{\mu^2 + ja} d\mu = 2e^{jk\rho a} \sqrt{\frac{\pi}{a}} \int_{\sqrt{k\rho a}}^{\infty} e^{-j\tau^2} d\tau \longrightarrow F[k\rho a]$$

Fresnel transition
function

SDP CONTRIBUTION

Uniform evaluation

$$\frac{1}{8\pi j} \int_{SDP_{\pm\pi}} S_1(\alpha) e^{-jk\rho \cos \alpha} d\alpha = \frac{e^{-j\pi/4}}{4\sqrt{2\pi}} \cot\left(\frac{\pi \pm \Phi^-}{4}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^\pm(\Phi^-)]$$

$$\frac{1}{8\pi j} \int_{SDP_{\pm\pi}} S_2(\alpha) e^{-jk\rho \cos \alpha} d\alpha = \frac{e^{-j\pi/4}}{4\sqrt{2\pi}} \cot\left(\frac{\pi \pm \Phi^+}{4}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^\pm(\Phi^+)]$$

$$F[k\rho g^\pm(x)] = j \underbrace{[f(\alpha_s) - f(\alpha_i)]}_{\text{Distance between saddle points and poles (angular separation)}} = 2j |\sqrt{k\rho g^\pm(x)}| \int_{\sqrt{k\rho g^\pm(x)}}^{\infty} e^{-j\tau^2} d\tau$$

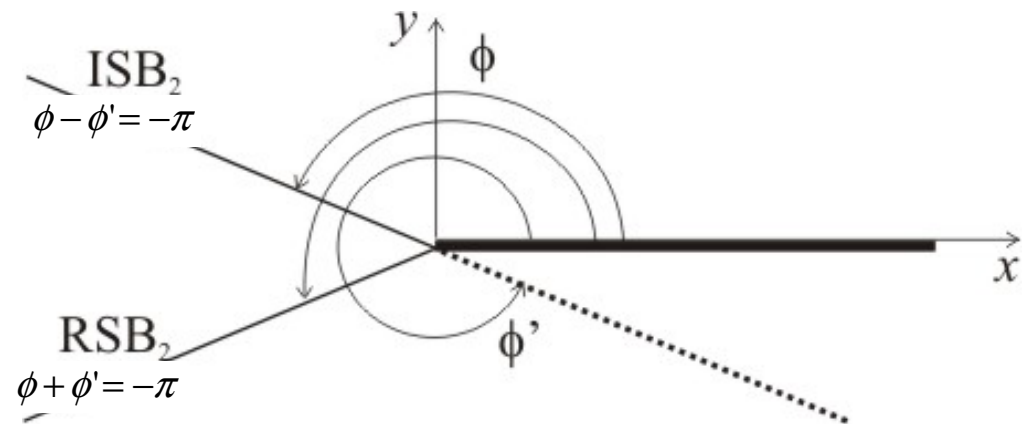
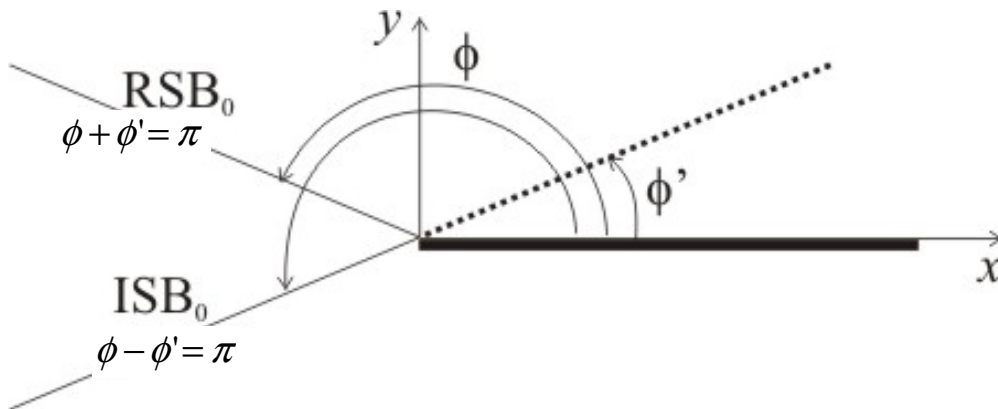
Distance between saddle points
and poles (angular separation)

$$g^\pm(x) = 1 + \cos[x - 4\pi N^\pm] \quad N^\pm \text{integer:} \quad \begin{cases} 4\pi N^+ - x = \pi \\ 4\pi N^- - x = -\pi \end{cases}$$

TOTAL RADIATED FIELD

GEOMETRICAL OPTICS FIELDS

<i>Incident GO</i>	<i>Reflected GO</i>		
$F_{GO}(k\rho) = \begin{cases} e^{jk\rho\cos(\phi-\phi')} \pm e^{jk\rho\cos(\phi+\phi')} \\ e^{jk\rho\cos(\phi-\phi')} \\ 0 \end{cases}$		$0 < \phi < \pi - \phi' \rightarrow \text{ISB}_0$	$\phi - \phi' = \pi$
		$\pi - \phi' < \phi < \pi + \phi' \rightarrow \text{RSB}_0$	$\phi + \phi' = \pi$
		$\pi + \phi' < \phi < 2\pi$	



TOTAL RADIATED FIELD

DIFFRACTED FIELDS

$$F_D(k\rho) = -\frac{e^{-j\pi/4}}{4\sqrt{2\pi}} \cot\left(\frac{\pi - \Phi^-}{4}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^-(\Phi^-)] \mp \frac{e^{-j\pi/4}}{4\sqrt{2\pi}} \cot\left(\frac{\pi - \Phi^+}{4}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^-(\Phi^+)] -$$
$$-\frac{e^{-j\pi/4}}{4\sqrt{2\pi}} \cot\left(\frac{\pi + \Phi^-}{4}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^+(\Phi^-)] \mp \frac{e^{-j\pi/4}}{4\sqrt{2\pi}} \cot\left(\frac{\pi + \Phi^+}{4}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^+(\Phi^+)]$$

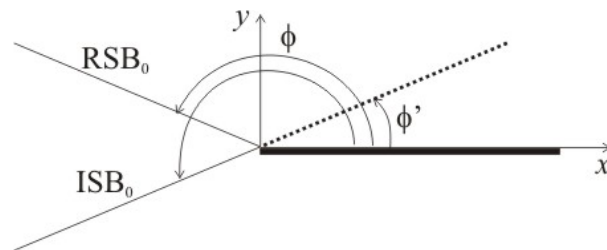
ISB face 0 RSB face 0

ISB face 2 RSB face 2

GENERALIZATION TO A PERFECTLY CONDUCTING WEDGE

$$F_D(k\rho) = -\frac{e^{-j\pi/4}}{2n\sqrt{2\pi}} \cot\left(\frac{\pi - \Phi^-}{2n}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^-(\Phi^-)] \mp \frac{e^{-j\pi/4}}{2n\sqrt{2\pi}} \cot\left(\frac{\pi - \Phi^+}{2n}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^-(\Phi^+)] -$$
$$-\frac{e^{-j\pi/4}}{2n\sqrt{2\pi}} \cot\left(\frac{\pi + \Phi^-}{2n}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^+(\Phi^-)] \mp \frac{e^{-j\pi/4}}{2n\sqrt{2\pi}} \cot\left(\frac{\pi + \Phi^+}{2n}\right) \frac{e^{-jk\rho}}{\sqrt{k\rho}} F[k\rho g^+(\Phi^+)]$$

TOTAL RADIATED FIELD



$$\phi' = 30^\circ$$

$$RSB_0 = 150^\circ$$

$$ISB_0 = 210^\circ$$

